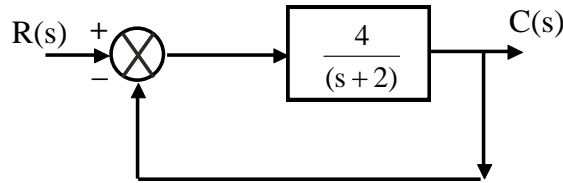




- Notes :
1. All questions carry marks as indicated.
 2. Due credit will be given to neatness and adequate dimensions.
 3. Assume suitable data wherever necessary.

1. Consider the system shown below. 16

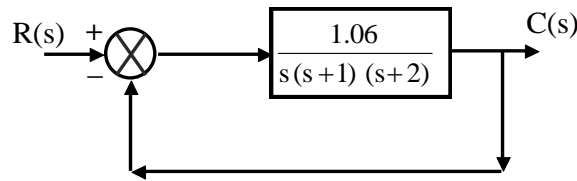


Design a Lead compensator to satisfy following specifications.

- 1) Damping factor $\xi = 0.5$
- 2) Undamped natural frequency $\omega_n = 4 \text{ rad/sec}$
- 3) Velocity error constant $k_v = 5 \text{ sec}^{-1}$

OR

2. Consider the system shown below. 16



Design a Lag compensator to satisfy following specifications.

- 1) Damping ratio $\xi = 0.491$
- 2) Undamped natural frequency $\omega_n = 0.673 \text{ rad/sec}$
- 3) Velocity error constant $k_v = 5.12 \text{ sec}^{-1}$.

3. The given open loop T.F. is : $G(s) = \frac{4}{s(s+2)}$. Design a lead compensator for closed – 16

loop system so that static velocity error constant $k_v = 20 \text{ sec}^{-1}$, phase margin is at least 50° , and gain margin is at least 10 dB.

OR

4. The given open – loop T.F. is : $G(s) = \frac{1}{s(s+1)(0.5s+1)}$. Design a lag compensator for 16

closed – loop system so that static velocity error constant k_v is 5 sec^{-1} , phase margin is at least 40° , and gain margin is at least 10 dB.

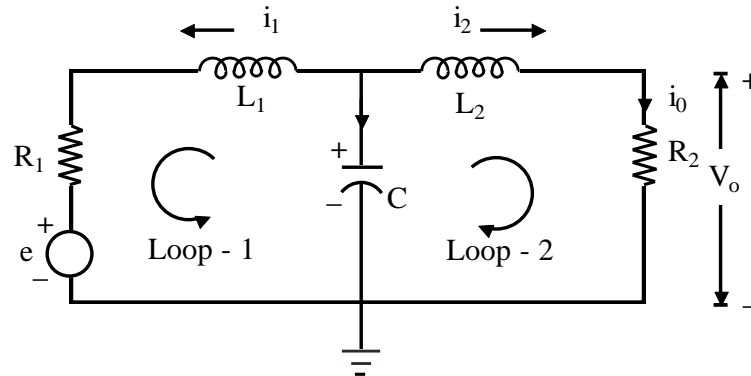
5. a) Explain designing of PID controller using frequency response approach. 8

- b) A forward path T.F. of unity closed – loop system is $G(s) = \frac{100}{(s+1)(s+5)(s+10)}$, required 8

$e_{ss} \leq 0.08$ for a unit ramp and phase margin $> 50^\circ$ at a frequency of 6 rad/sec . Determine a PID controller.

OR

6. a) Derive the T.F. of electronic PI controller using Op-Amp. 8
 b) Discuss the Ziegler – Nicholes PID controller tuning methods. 8
7. a) Obtain the state – space representation of Armature – controlled DC motor. 8
 b) Obtain state – space representation of RLC network given below. 8



OR

8. a) Derive the solution of Homogeneous state equation. 8
 b) Obtain time response of the system described by 8

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -6 & -5 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u \text{ \& } y = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

when $u = 1$ for $t \geq 0$ and $\begin{bmatrix} x_1(0) \\ x_2(0) \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$.

9. a) Define the controllability and derive the condition for controllability. 8
 b) Consider the system described by 8

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -5 & -6 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u$$

By using state feedback control $u = -KX$, it is desired to have closed – loop poles at $S_1 = -2 + j4, S_2 = -2 - j4, S_3 = -10$. Determine state feedback matrix K .

OR

10. a) Define the observability and derive the condition for observability. 8
 b) Consider the system described by 8

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -2 & -3 & -5 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u \text{ \& } y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

By using state feedback control $u = -KX$, it is desired to have closed-loop poles at $S_1 = -4.80 + j3.60, S_2 = -4.80 - j3.60, S_3 = -4.80$. Determine state feedback matrix.
